RADIO ATTACKS ON NFC, GPS, AND MOBILES

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SDR SOFTWARE-DEFINED RADIO

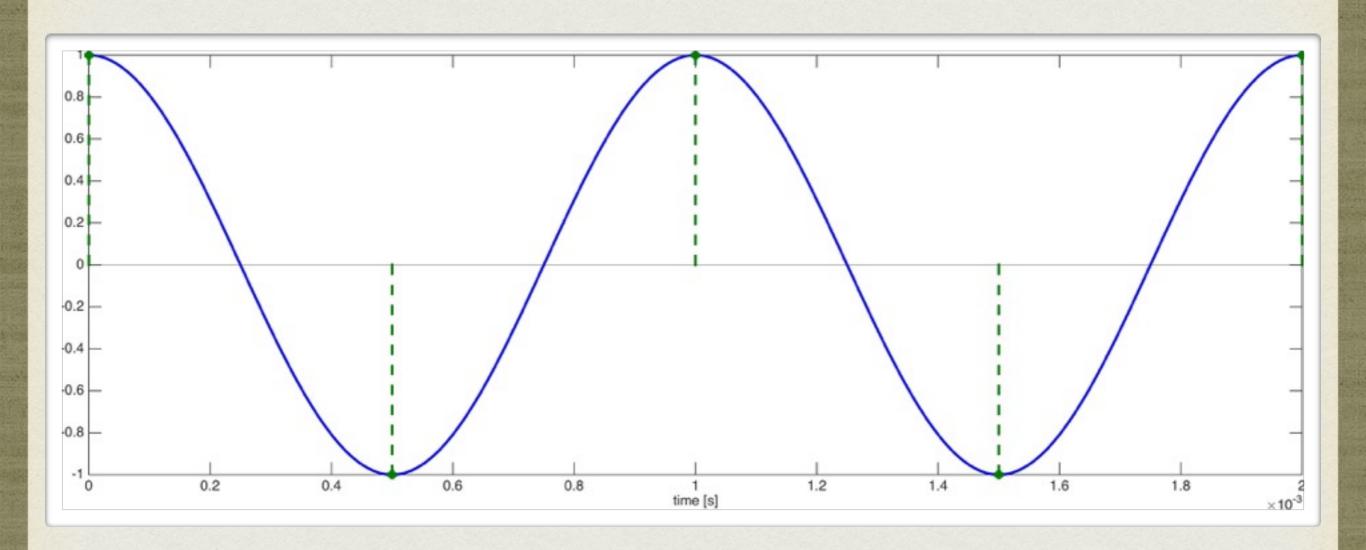
SAMPLING THEOREM

- Let s(t) be a Fourier-integrable signal having its highest non-negligible frequency $|f_{\text{max}}| < f_{\text{s}}/2 = 1/2T_{\text{s}}$.
- Such *s*(*t*) can be then fully reconstructed from its discrete-time samples as:

$$s(t) = \sum_{k=-\infty}^{\infty} s(kT_s) \frac{\sin \pi (\frac{t - kT_s}{T_s})}{\pi (\frac{t - kT_s}{T_s})} = \sum_{k=-\infty}^{\infty} s(kT_s) \operatorname{sinc}(\frac{t - kT_s}{T_s})$$

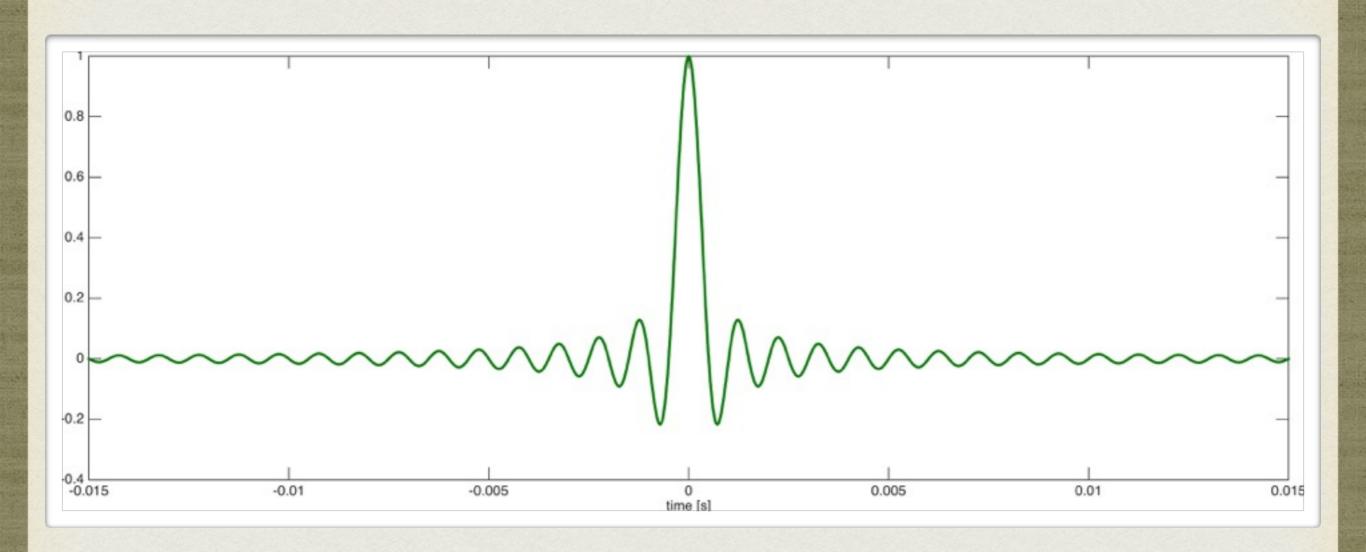
- Kotelnikov, Nyquist, Shannon, Whittaker

NYQUIST RATE SAMPLING



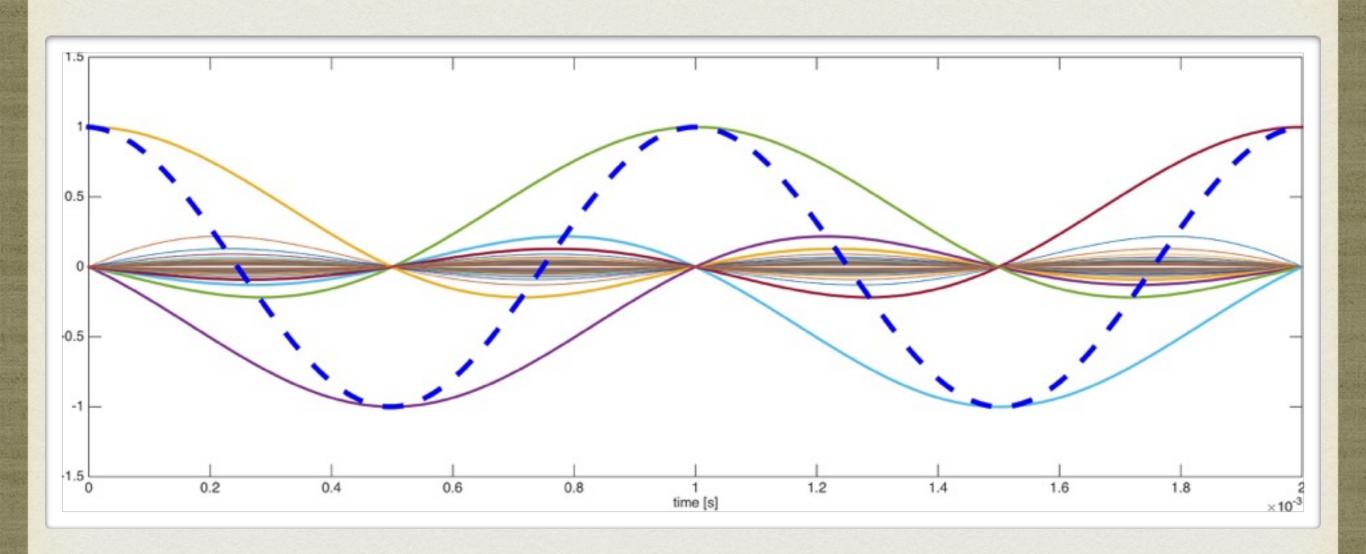
1 kHz @ Nyquist sample rate fs = 2 kHz

SINUS CARDINALIS



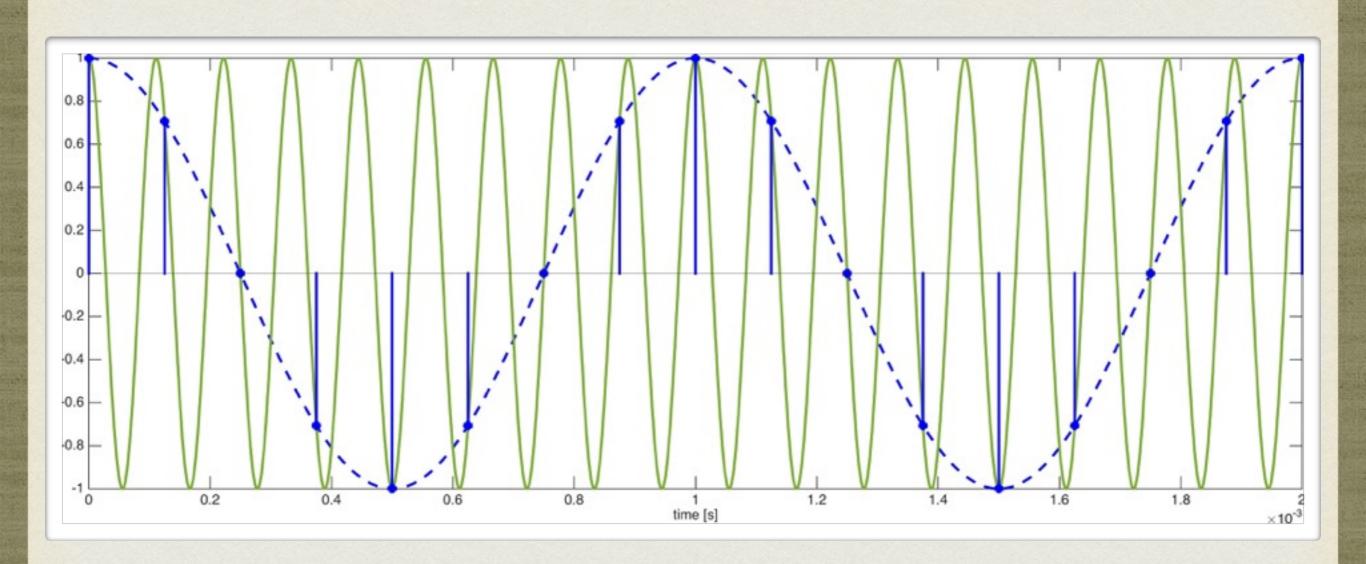
in lowpass filter impulse response scale @ 1 kHz

INTERPOLATION



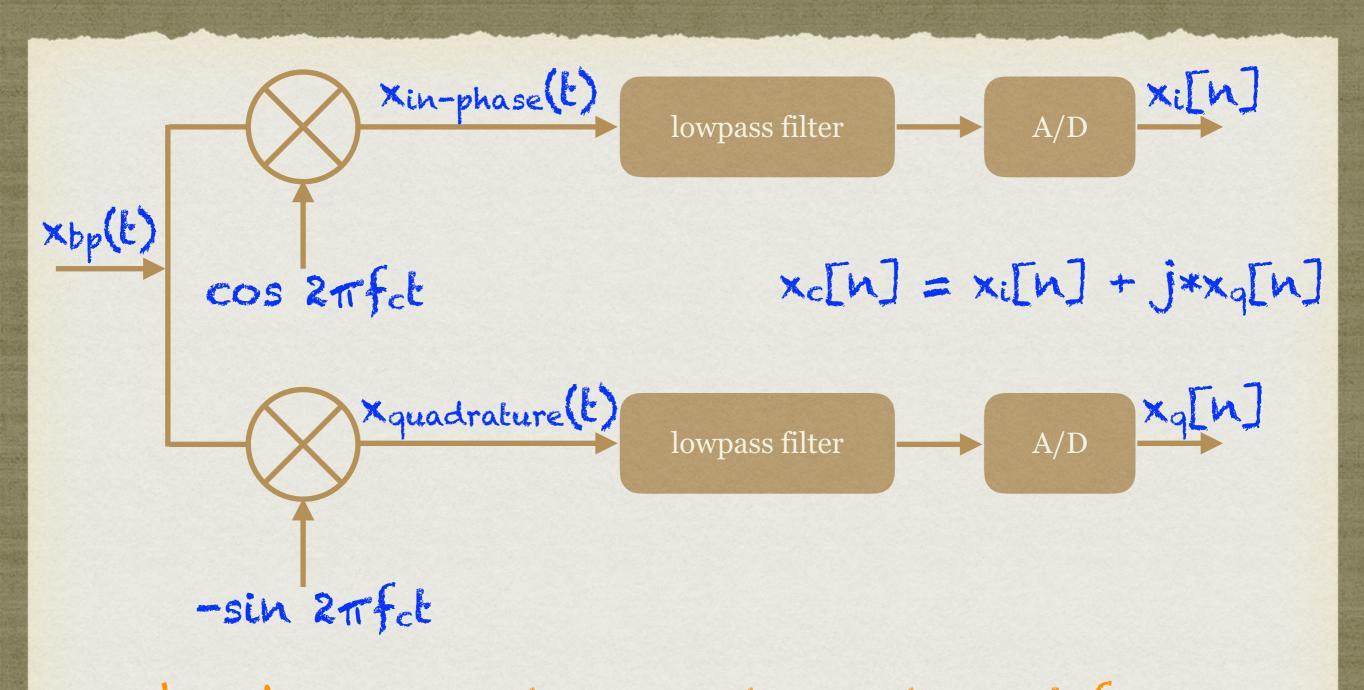
1 kHz recovered @ fs = 2 kHz with 30-sample delay

ALIASING EXAMPLE



9 kHz -> 1 kHz @ sample rate fs = 8 kHz

QUADRATURE SAMPLING



bandpass complex signal sampling at fs = B

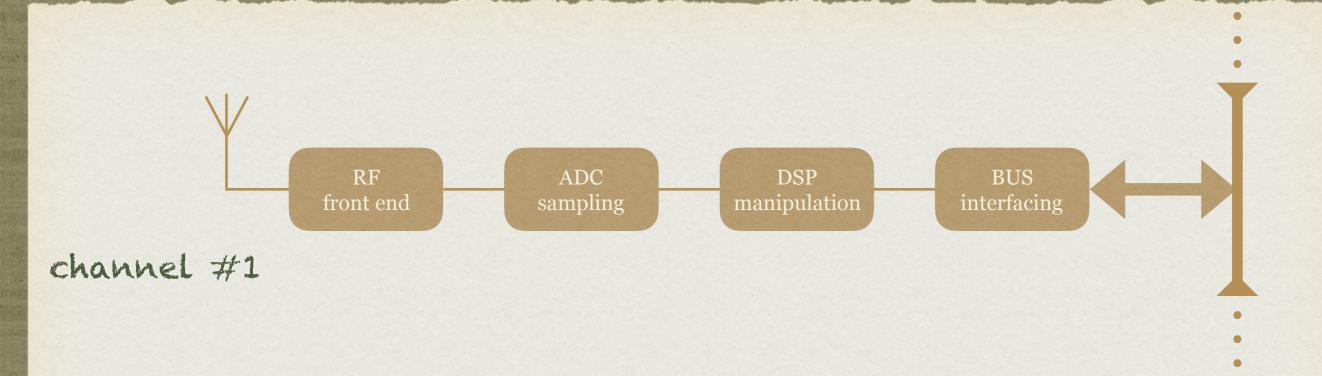
cf. [Lyons, 2011] for excellent explanation

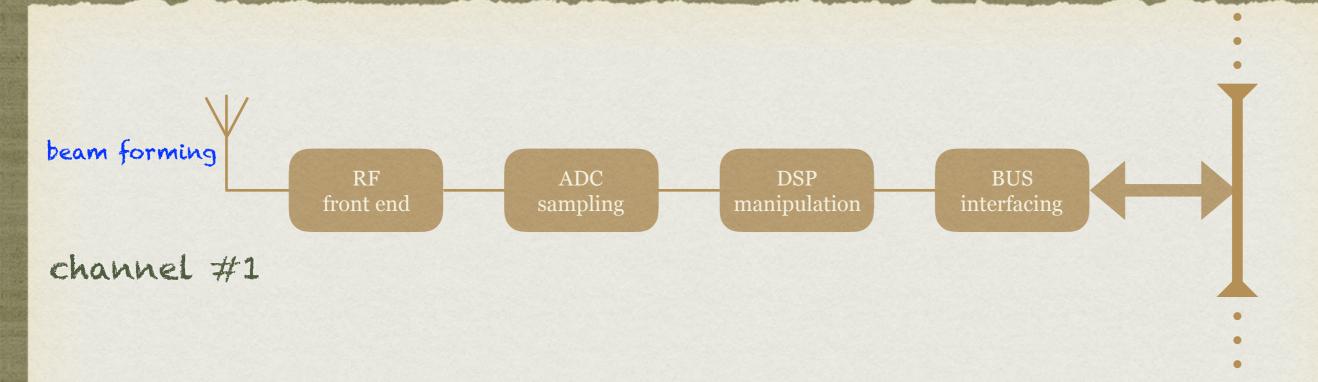
DIGITAL SIGNAL PROCESSING (DSP)

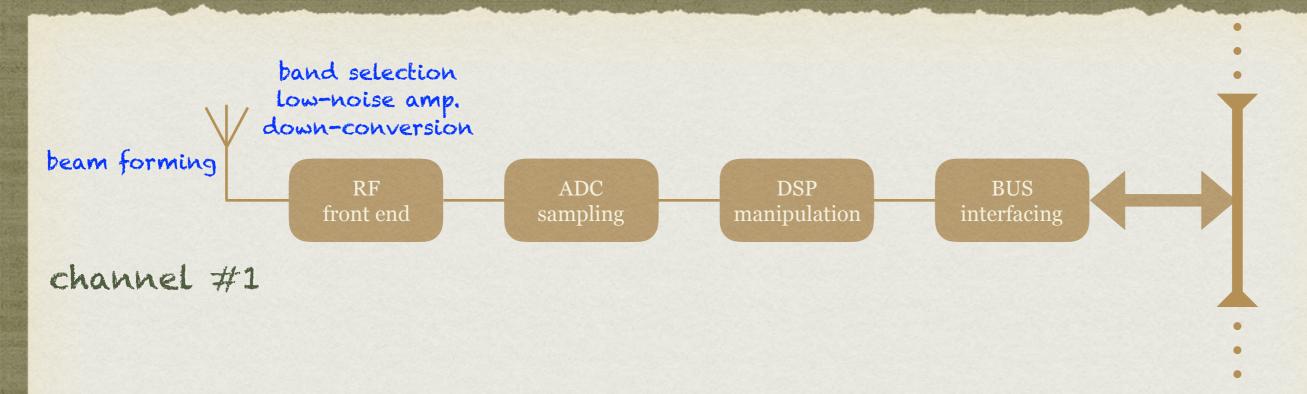
... (thanks to the sampling theorem), uses the correspondence of continuous-time functions and discrete-time sequences to process the input signals by digital operations instead of analog circuits

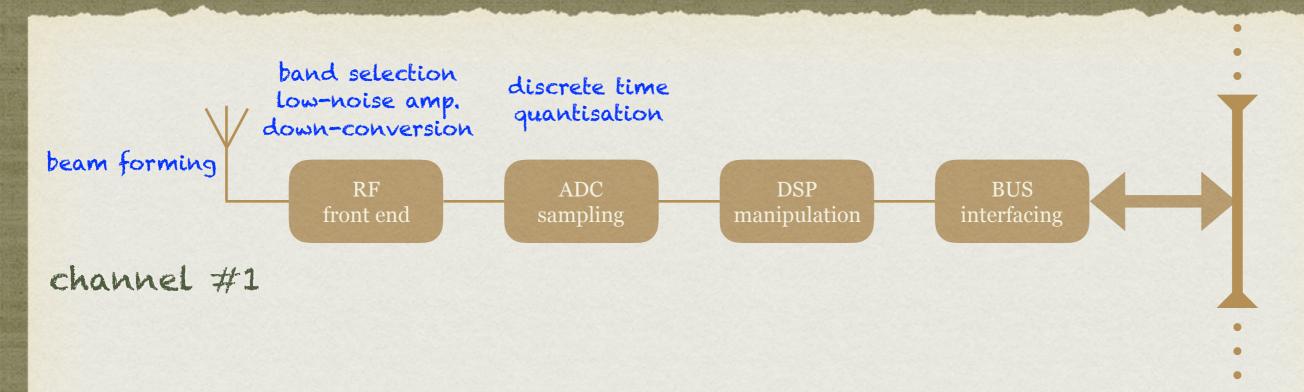
SOFTWARE-DEFINED RADIO (SDR)

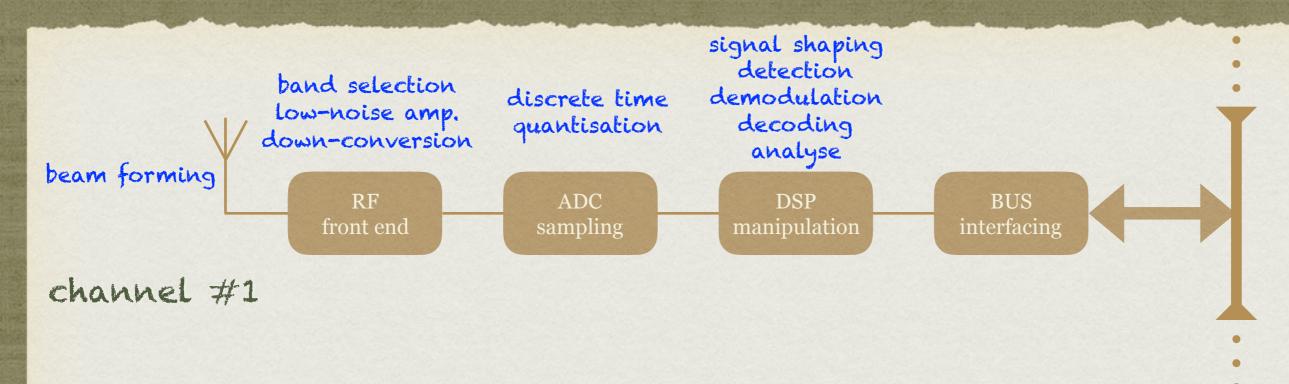
... (thanks to the digital signal processing), components that have been typically implemented in (analog) hardware are instead implemented by means of software on a personal computer or embedded system

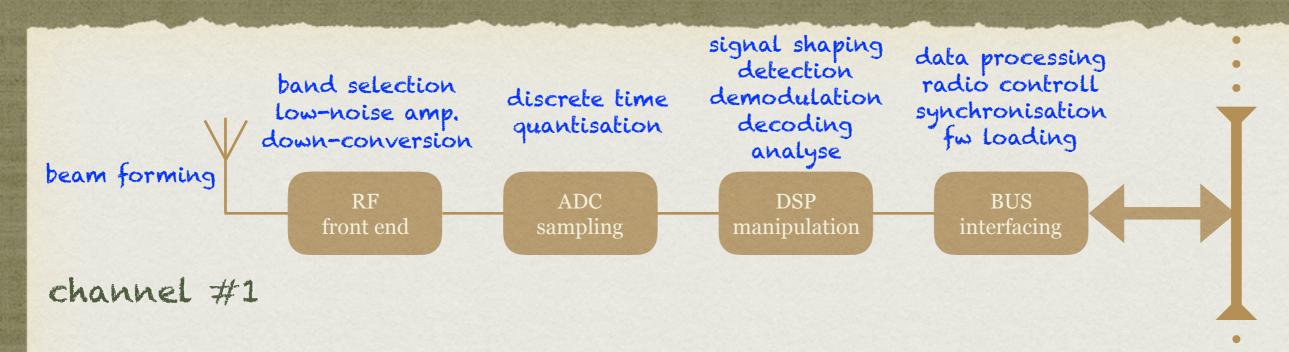


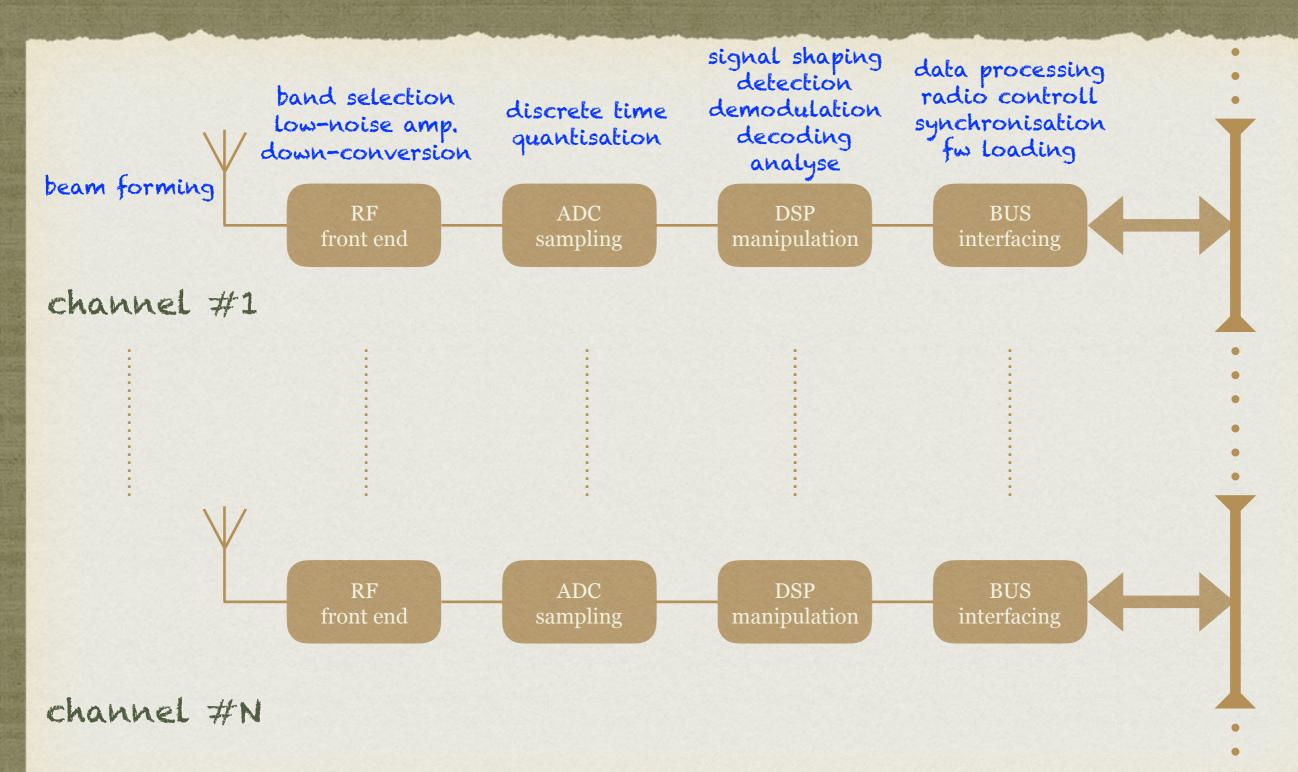


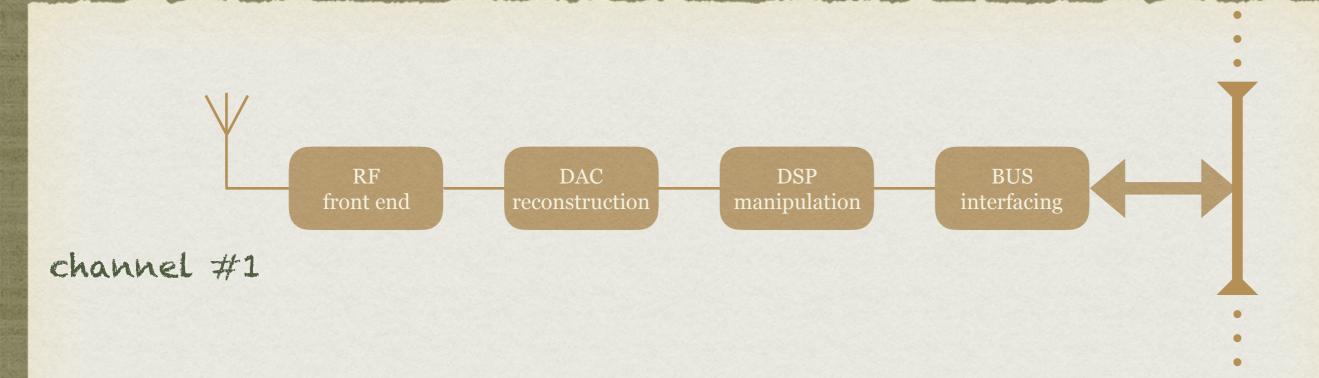


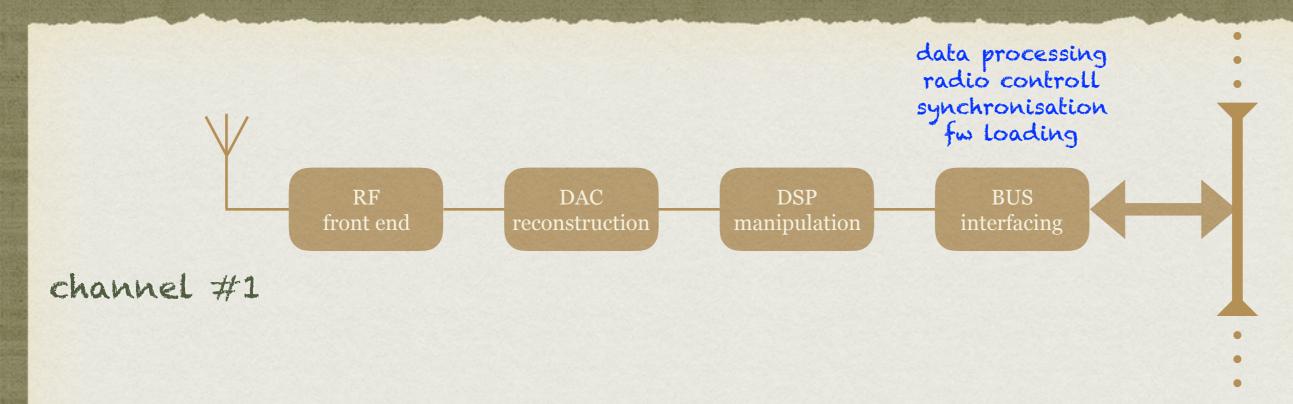


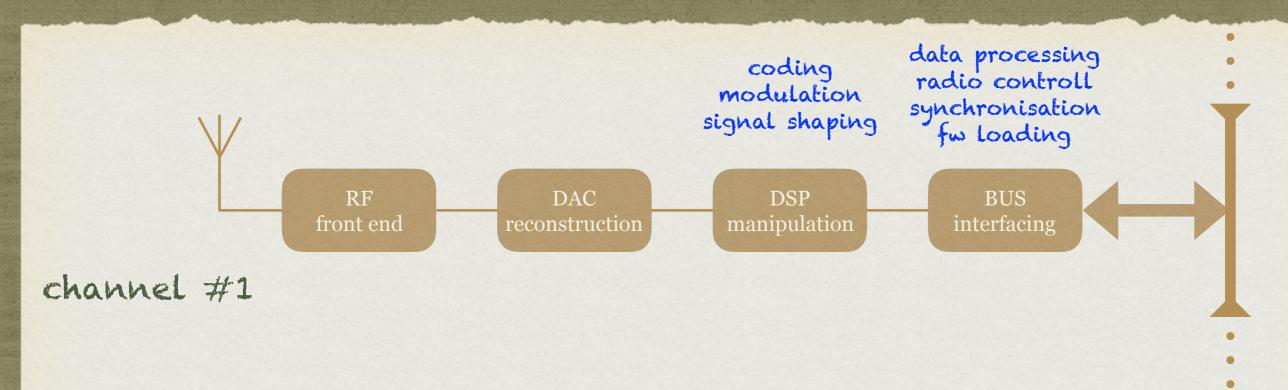


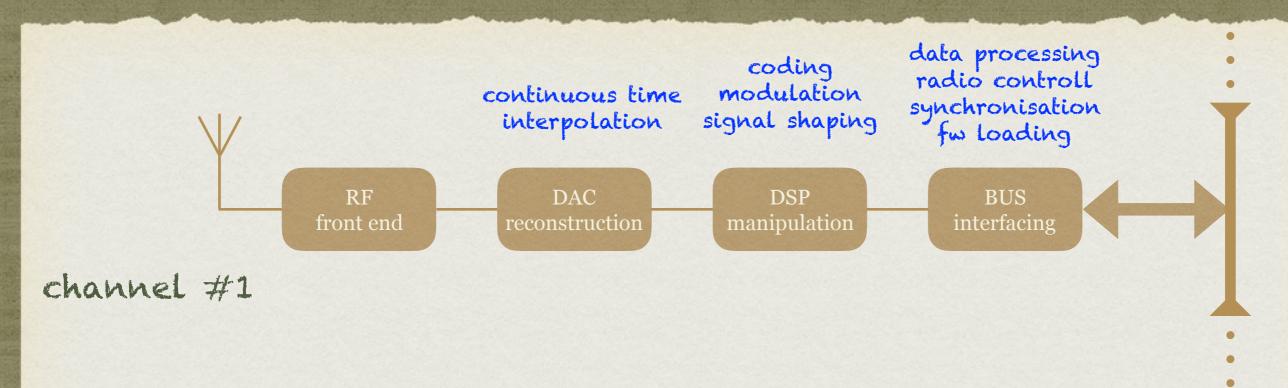


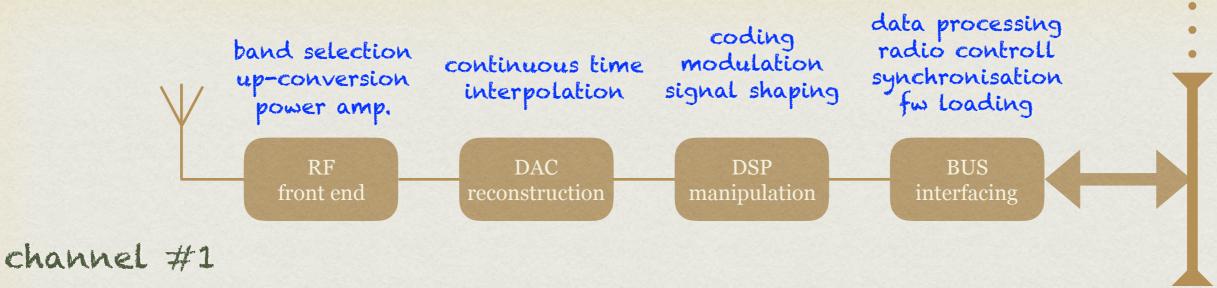


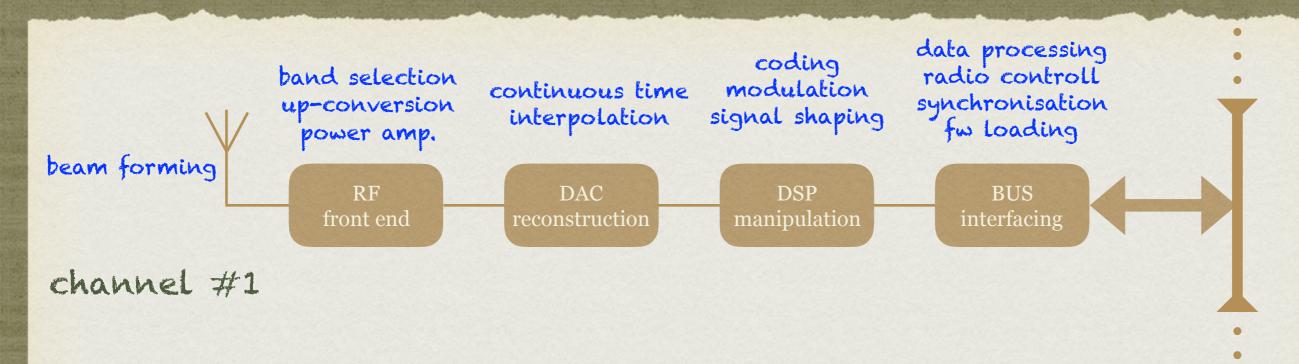


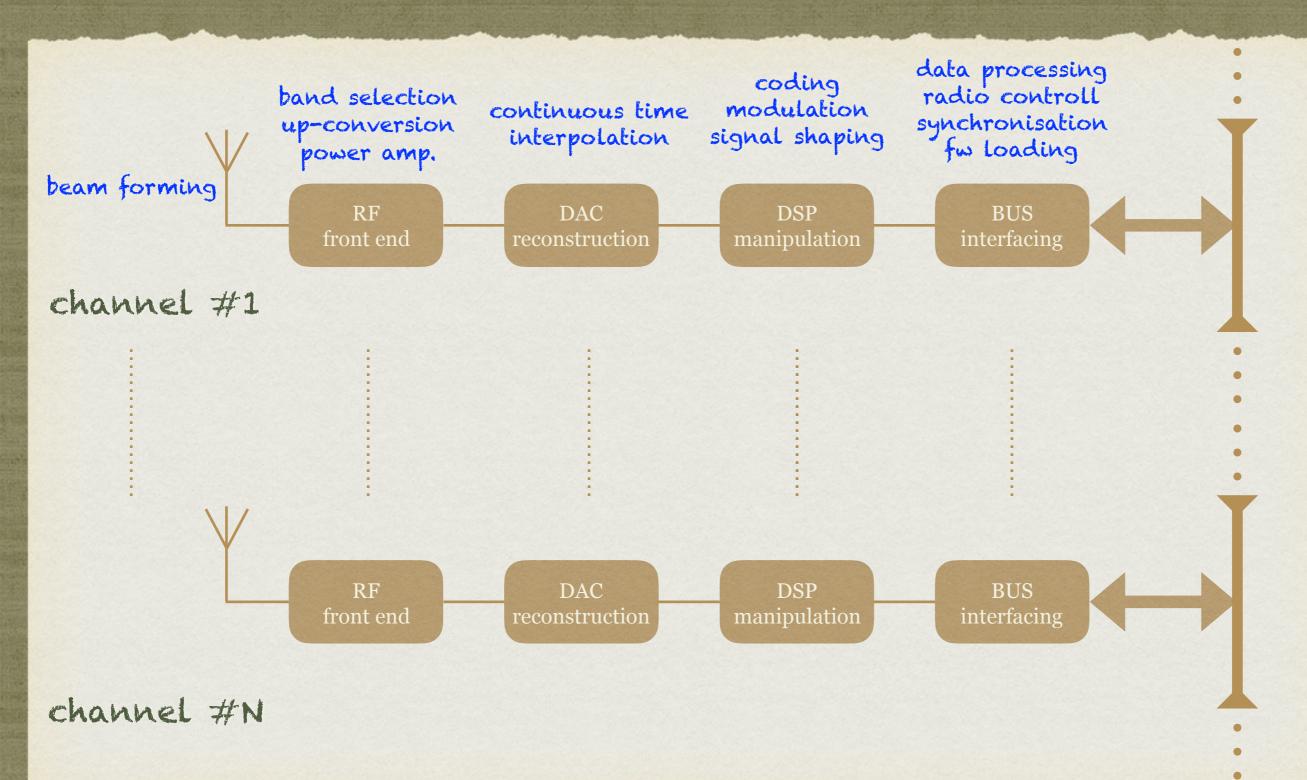








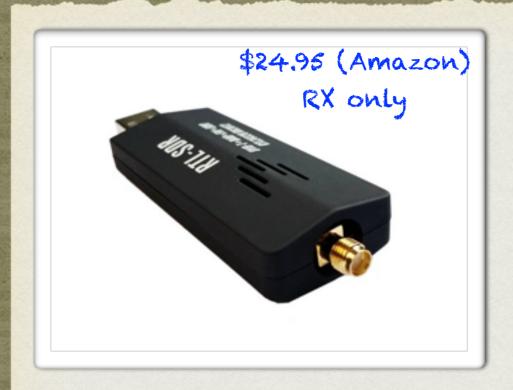


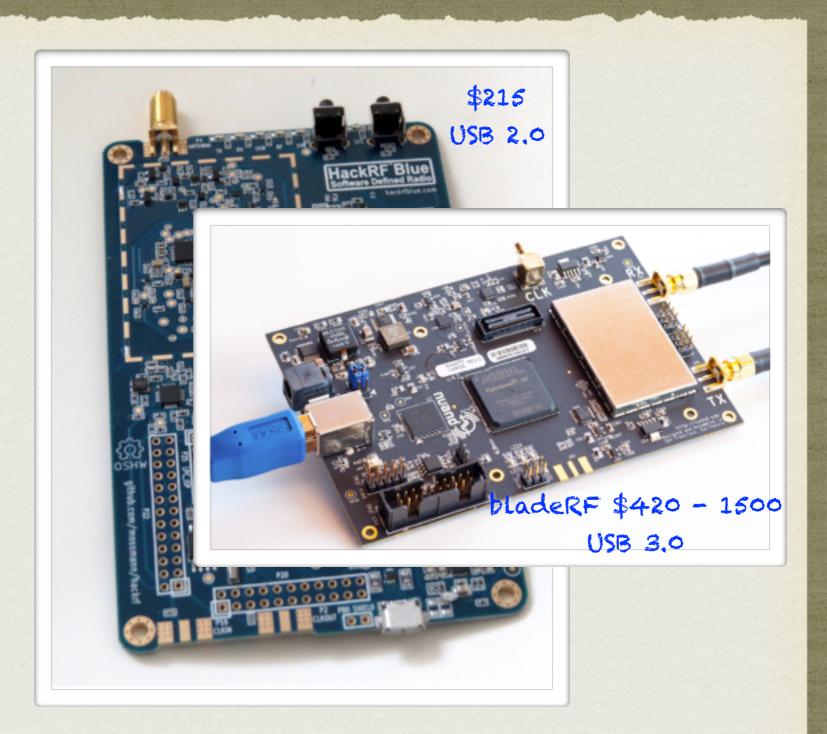




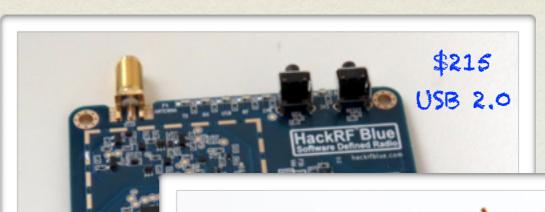


















SDR AS A THREAT

DSP routines are SW. This can be shared, installed, and executed all around the world instantly with a very modest background.

Just like any other exploit code.

NFC NEAR FIELD COMMUNICATION

START WITH SOMETHING FAMILIAR



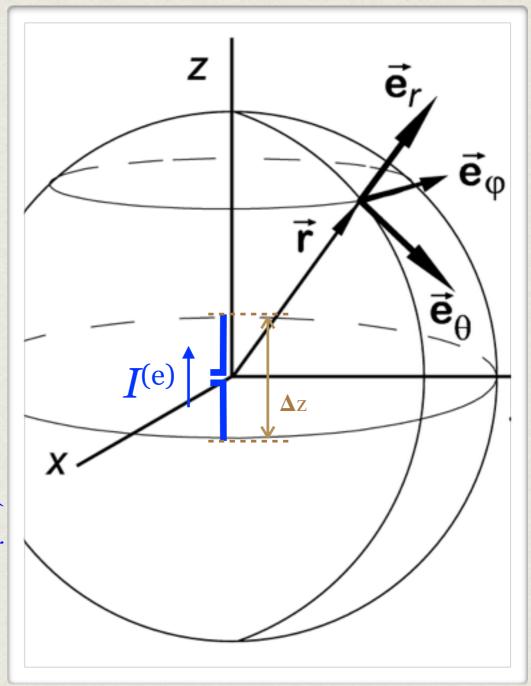
[Buddipole QRV by 5B8AP]

THE IDEAL ELECTRIC DIPOLE

- Electrically small, i.e. $\Delta z << \lambda$, uniform amplitude current element.
 - Ordinary dipole is covered by integration over these elements.
- In the far field, a donut-like pattern bearing the vertical polarisation is produced.
- In general, its field has the following components.

$$\overrightarrow{E}_{edp}(I^{(e)}) = E_{edp,\theta}(I^{(e)}) \cdot \widehat{e_{\theta}} + E_{edp,r}(I^{(e)}) \cdot \widehat{e_{r}}$$

$$\overrightarrow{H}_{edp}(I^{(e)}) = H_{edp,\phi}(I^{(e)}) \cdot \widehat{e_{\phi}}$$



(illustration purpose only)

LONG STORY SHORT

$$\vec{H}_{edp}(I^{(e)}) = \frac{I^{(e)}\Delta z}{4\pi} j\beta(\frac{1}{r} + \frac{1}{j\beta r^2})e^{-j\beta r}\sin\theta \cdot \hat{e}_{\phi}$$

$$\vec{E}_{epd}(I^{(e)}) = \frac{I^{(e)}\Delta z}{4\pi} j\omega\mu(\frac{1}{r} + \frac{1}{j\beta r^2} - \frac{1}{\beta^2 r^3})e^{-j\beta r}\sin\theta \cdot \hat{e}_{\theta}$$
$$+ \frac{I^{(e)}\Delta z}{2\pi} j\omega\mu(\frac{1}{j\beta r^2} - \frac{1}{\beta^2 r^3})e^{-j\beta r}\cos\theta \cdot \hat{e}_{r}$$

$$= \frac{I^{(e)} \Delta z}{4\pi} j\omega \mu (\frac{1}{r} + \frac{1}{j\beta r^{2}} - \frac{1}{\beta^{2} r^{3}}) e^{-j\beta r} \sin \theta \cdot \hat{e}_{\theta}$$
$$+ \frac{I^{(e)} \Delta z}{2\pi} \eta (\frac{1}{r^{2}} - j\frac{1}{\beta r^{3}}) e^{-j\beta r} \cos \theta \cdot \hat{e}_{r}$$

TOWARDS SOMETHING APPEALING



[AlexLoop by Alex, PY1AHD]

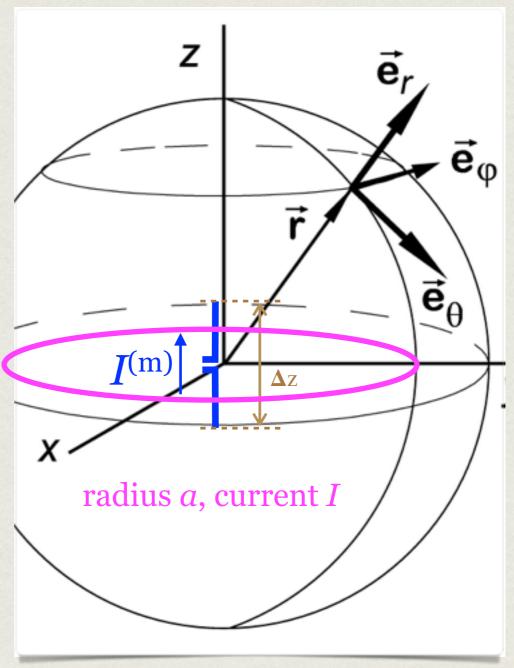
THE SMALL LOOP

- Electrically small, i.e. $2\pi a < \lambda/10$, uniform amplitude current loop.
- Can be modelled as an ideal *magnetic* dipole which is the theoretical dual of the ideal electric dipole.
- The duality equations follow.

$$\vec{E}_{mdp}(I^{(m)}) \equiv -\vec{H}_{edp}(I^{(m)}), \vec{H}_{mdp}(I^{(m)}) \equiv \vec{E}_{edp}(I^{(m)})$$

$$\mu_{mdp} \equiv \varepsilon_{edp}, \varepsilon_{mdp} \equiv \mu_{edp}$$

$$\beta_{mdp} = \omega \sqrt{\mu_{mpd}} \varepsilon_{mdp} = \omega \sqrt{\varepsilon_{edp}} \mu_{edp} = \beta_{edp}$$
note also $\beta = \frac{2\pi}{\lambda}, v = \lambda f$



(illustration purpose only)

LONG STORY SHORT

$$\vec{E}_{mdp}(I^{(m)}) = -\frac{I^{(m)}\Delta z}{4\pi} j\beta(\frac{1}{r} + \frac{1}{j\beta r^2})e^{-j\beta r}\sin\theta \cdot \hat{e}_{\phi}$$

$$\vec{H}_{mpd}(I^{(m)}) = \frac{I^{(m)}\Delta z}{4\pi} j\omega \varepsilon (\frac{1}{r} + \frac{1}{j\beta r^2} - \frac{1}{\beta^2 r^3}) e^{-j\beta r} \sin\theta \cdot \hat{e}_{\theta}$$
$$+ \frac{I^{(m)}\Delta z}{2\pi} j\omega \varepsilon (\frac{1}{j\beta r^2} - \frac{1}{\beta^2 r^3}) e^{-j\beta r} \cos\theta \cdot \hat{e}_{r}$$

MAGNETIC CURRENT OF THE SMALL LOOP

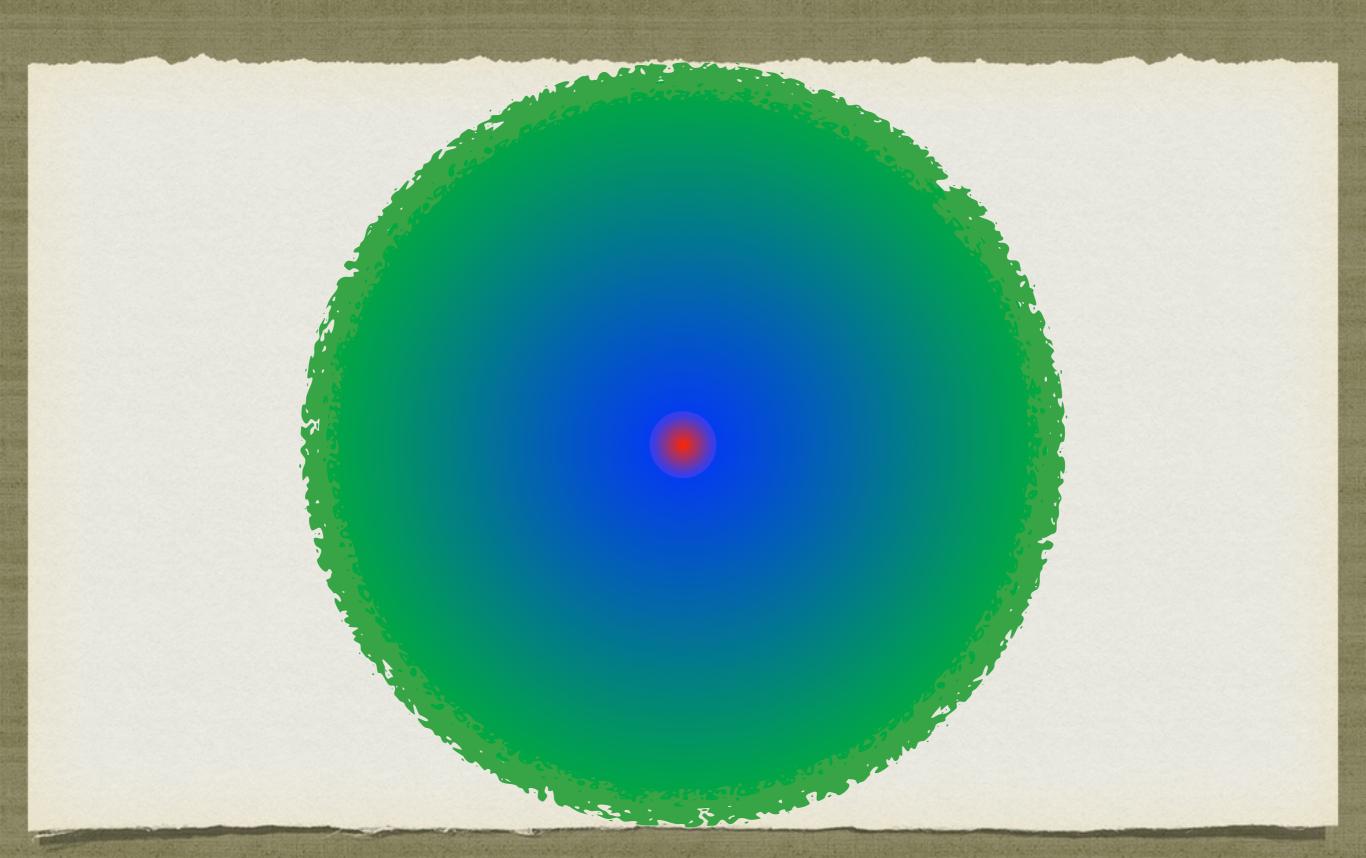
$$I^{(m)}\Delta z = j\omega \mu IS$$
$$S = \pi a^2$$

(based on far field equivalence)

NEAR, FAR

- Basing on the different dominating *E*, *H* field terms implying *different* dominating field behaviour, it is useful to distinguish:
 - Reactive near field (XNF), where the terms with $1/r^2$ and $1/r^3$ dominate. Energy is mainly stored and exchanged between E and H.
 - Radiating near field (Fresnel region), where the $1/r^2$ terms start to dominate, i.e. $r > \lambda/2\pi$. Energy is mainly radiated with unstable patterns, however.
 - Far field (Fraunhofer region), where the 1/r terms remain to dominate and the plane wave model can be used. Several conditions shall be met: $r > 2D^2/\lambda$, r > 5D, $r > 1.6\lambda$, where D is the largest antenna dimension. Energy is radiated with a distance-independent field pattern.

WHEREVER YOU ARE



ANTENNA IMPEDANCE

$$Z_A = R_r + R_o + jX_A$$

- The input impedance Z_A describes the antenna from the lumped circuit parameters viewpoint. This is also useful to describe the antenna field action observable in those different field regions in a handy condensed way.
 - $R_{\rm r}$ is the equivalent radiation resistance representing the energy emanated through the radio waves
 - R_0 describes the dissipative energy loss
 - X_A reflects the energy exchanged back-and-forth with the reactive near field

RADIATION OF THE SMALL LOOP

$$P = 10I^{2}(\beta^{2}S)^{2}$$

$$R_{r} = \frac{2P}{I^{2}} = 20(\beta^{2}S)^{2} \approx 31171(\frac{S}{\lambda^{2}})^{2}$$

$$\approx 31171(\frac{NS}{\lambda^{2}})^{2}, \text{ for a small } N\text{-turn loop}$$

DAMPING RESISTOR

- For the radiation efficiency analysis, R_0 shall also cover any damping resistor R_q used.
- Especially for NFC, a nonzero R_q is often inserted serially to lower the antenna Q to achieve the required bandwidth.
 - Finally, we can expect a very small radiation efficiency for a typical NFC antenna.
 - Interestingly, we may investigate on how to design a yet-usable NFC antenna that is, however, a very poor radiator anyway.
 - Nevertheless, it does not mean the radiation is zero.

EFFICIENCY ANALYSIS

- To get a better overview, we can compute the radiation efficiency $e_{\rm r}$ that can be further used for e.g. gain estimation, etc.
- We do that by comparing the equivalent real resistances from the circuit model of Z_A .

$$R_s = \sqrt{\frac{\omega\mu}{2\sigma}}$$

$$R_o = \frac{a}{c} R_s$$
, a ~ loop radius, c ~ wire radius

$$e_r = \frac{R_r}{R_q + R_o + R_r}$$

YES, IT CAN!

- NFC antenna is generally capable of transmitting its signal into the far field region.
- Due to its construction, the radiation resistance is very small leading to a very poor energy transfer.
- Nevertheless, it does not mean there would be no transmission at all.

PARASITIC ANTENNAS

- From the security viewpoint, we shall recognise it may not be the *primary* antenna only that can radiate sensitive data.
- In general, any spatial distribution of a time-varying current modulated (or sensed!) by the internal processing unit is a potential backdoor.
 - We are getting to the well-known phenomenon of the electromagnetic sidechannels.
 - Here, we have an extremely high chance this mechanism is exploitable by attackers.
 - In principle, applying anti-RFI techniques for all those patch cables and power lines is a good idea to start with.

INITIATOR RANGE EXTENSION

- Allows RF skimming or wormhole (relay) attacks.
- Due to a very low efficiency and very high power consumption, it is practically limited to the reactive near field region (XNF).
- Antenna diversity separating downlink and uplink channels may help significantly.
- Distance: Decimetres (confirmed), reliably working at around 20 cm. Principal upper limit $\approx \lambda/2\pi$, i.e. circa 3.5 m, is infeasible to achieve practically. So, we are limited to a kind of *bumping* attack.

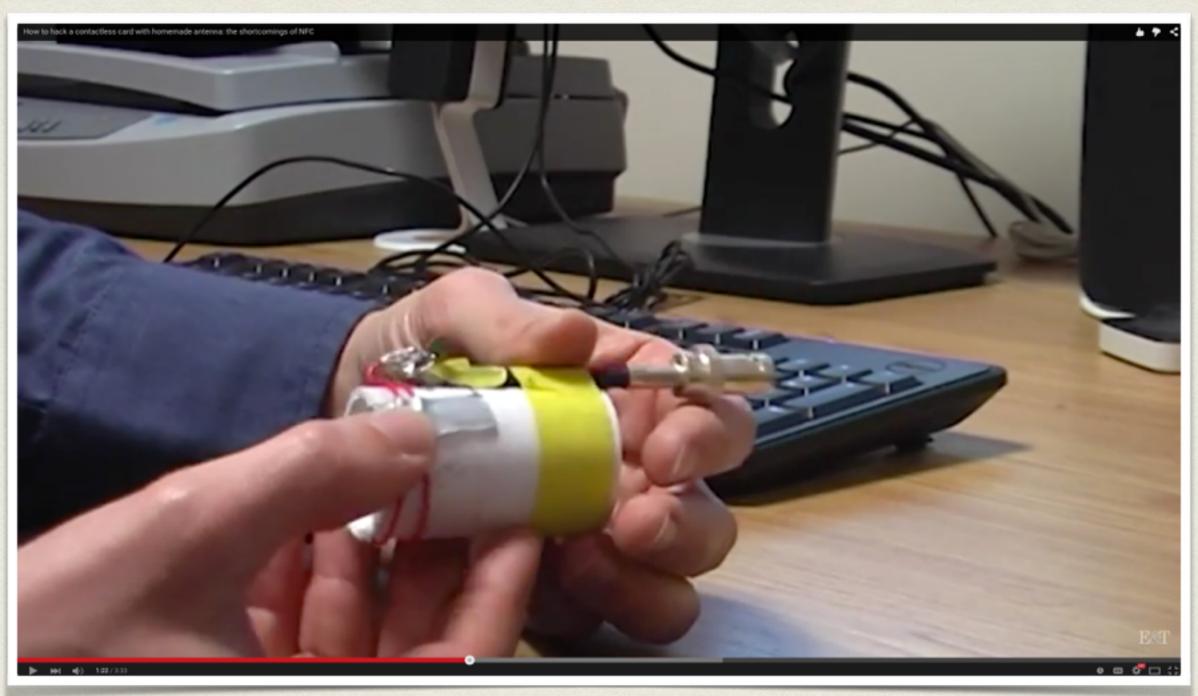
SNIFFING

- Sensitive data capture, identity theft.
- Works over all zones, from XNF to Fraunhofer region.
- Often, this scenario induces the most serious risks.
- For regions outside XNF, the important idea is to look for higher harmonics of the 13.56 MHz carrier.
- Furthermore, antenna design and orientation varies through the regions.
- Distance: Metres to dekametres. Confirmed for both downlink and uplink channels.

ALL YOU NEED IS LOOP



SPYING IN THE LANE (STILL IN XNF)



[https://www.youtube.com/watch?v=9QjxwejBPHs]

TARGET RANGE EXTENSION

- Allows covert communication with NFC terminal.
- Combines the techniques for a long range sniffing with the reciprocal problem of an extended-range signal injection into the RF front-end of the terminal.
- Based on direct DSB (Double Side Band) or even SSB (Single Side Band) injection, basing on the particular terminal signal processing.
- Principally possible even from the Fraunhofer region.
- The terminal antenna gain together with its input sensitivity limits the distance.
- Distance: Metres (confirmed). Working from the Fraunhofer region is practically very hard.

TRAFFIC INJECTION

- Allows Man-In-The-Middle scenarios.
- Due to the linear superposition in the EM field, the attacker does not have to be geometrically right in the middle, neither to break the original channel spatially.
- Again, a few turns of a wire around the original reader can be enough.
- Note we can also spoof the Initiator packets, besides the Target responses.
- Covering the path to the Target (downlink) requires XNF. One sided injection can work from the Fresnel or Fraunhofer regions as well.
- Distance: Decimetres (downlink TX covered) up to metres (TX for uplink only). Confirmed indirectly by other experiments together with own observations (cf. below).

INITIATOR LOCATION

- Allows searching for active terminals for instance, exposing passengers inspection, etc.
- Carrier detection at 13.56 MHz or higher harmonics, possibly also with the communication footprint.
- Distance: Dekametres. Indirectly confirmed by the eavesdropping experiments that can serve as a lower bound.

TARGET LOCATION

- Allows searching for potentially valuable assets.
- Searching based on radio characteristics without querying the higher protocol layers.
- Electronic Article Surveillance (EAS) style to search for the particular resonant circuits.
- Distance: Decimetres (confirmed by the range extension experiments) to metres (estimated).

JAMMING

- Allows DoS attacks at airport, office entry, market centre etc.
- We can use reciprocity theorems to estimate the effect an attacker's (measurement) antenna would have on the terminal input.
- Distance: Metres (confirmed by the range extension experiments) to dekametres (estimated).

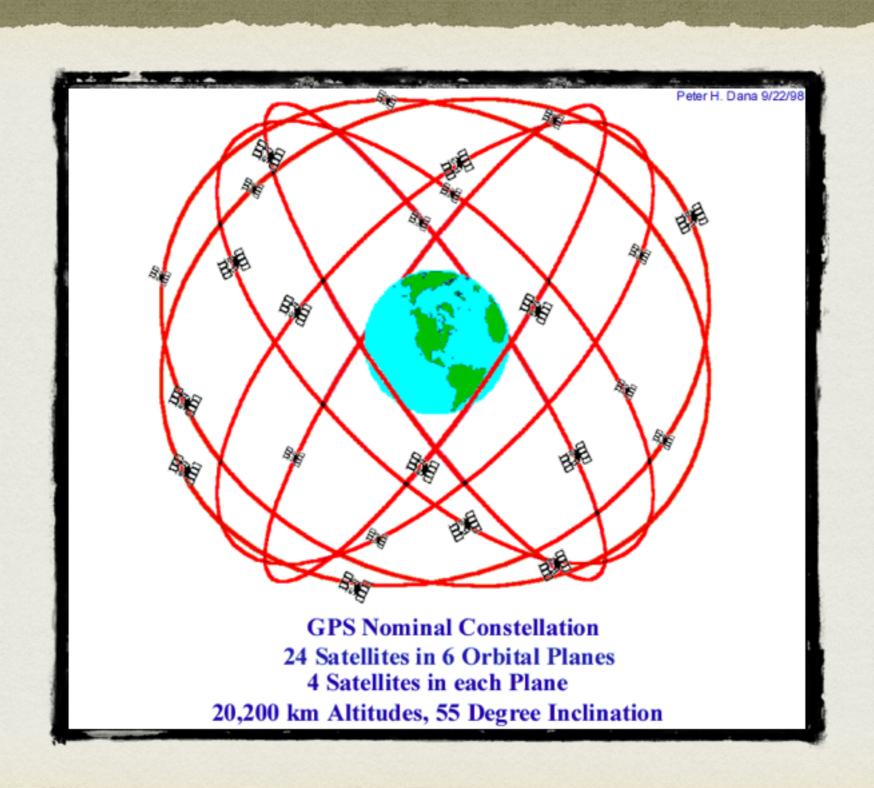
DEVICE DESTRUCTION

- Allows selective DoS on the terminal or transponder.
- In principle, it requires a strong power pulse, so a near field approach is assumed.
- Distance: Decimetres.

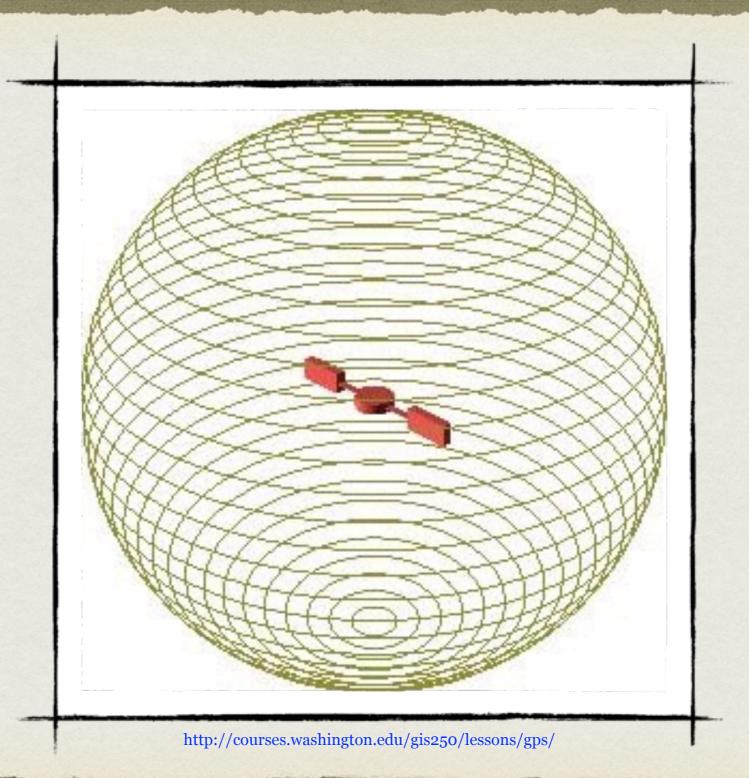
GPS GLOBAL POSITIONING SYSTEM



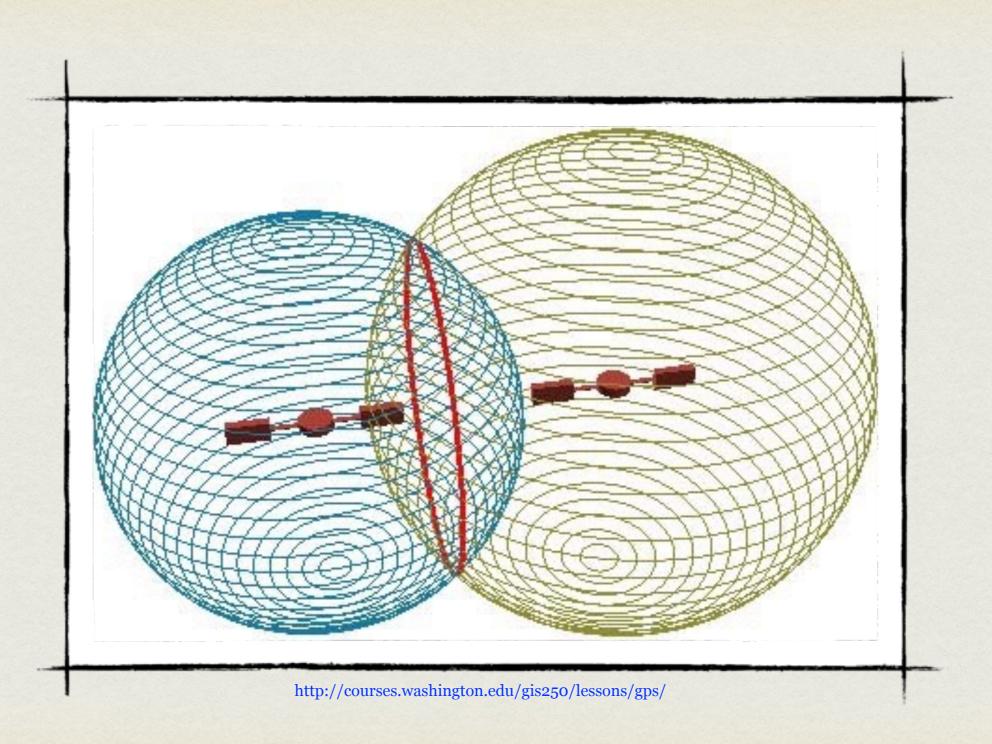
GPS SPACE SEGMENT



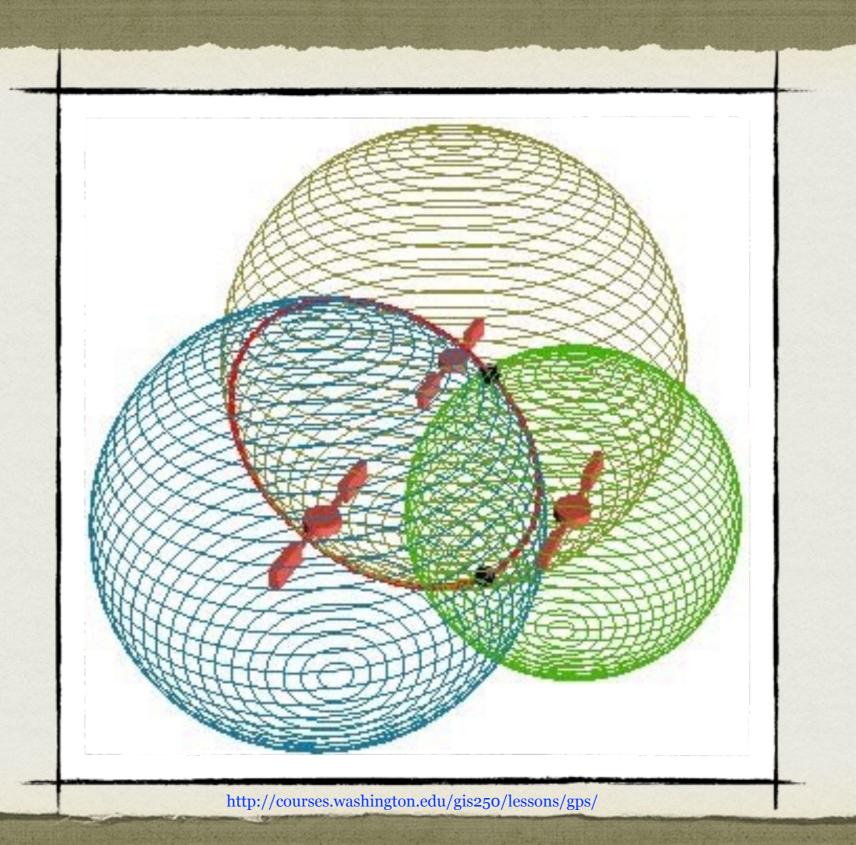
TRILATERATIONI



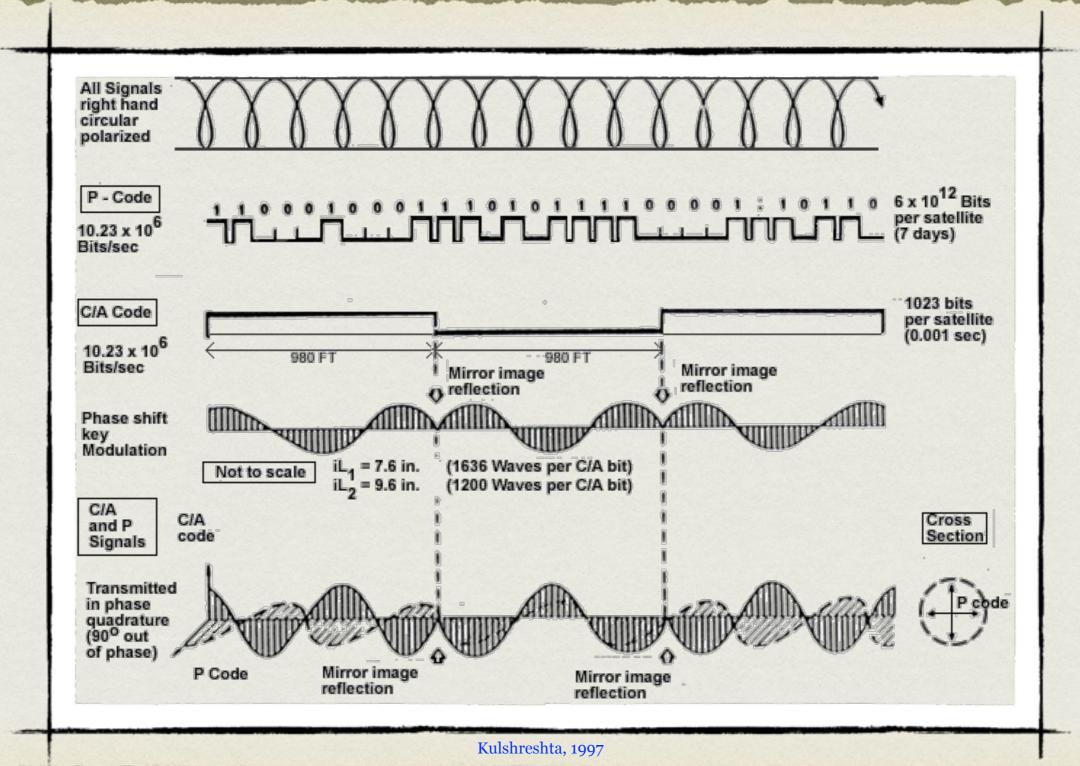
TRILATERATION II



TRILATERATION III



GPS L1 C/A & P(Y) (ILLUSTRATION ONLY)



SATELLITE CLOCK REPLICAS EXPOSE THE TIME DELAYS



tsent_sv1



tsent_sv2



tsent_sv3



four SVs to get X, Y, Z, and thias



trec+thias

CIVIL GPS IN SERIOUS APPLICATIONS





NTP server



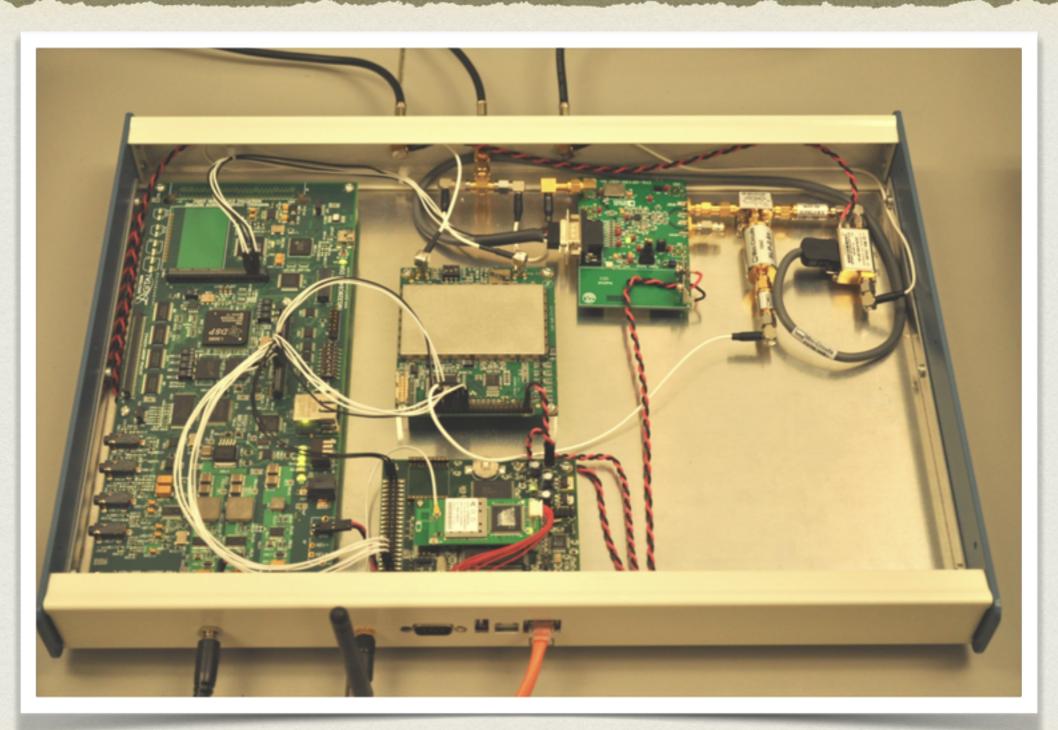
L1 C/A SIGNAL IN BRIEF

- CDMA at the common carrier frequency of 1575.42 MHz
- Satellites distinguished by their unique chipping sequence (Gold codes)
- Allows creation of a delayed replica clock of the particular satellite (implicit time synchronisation)
- Carries 37 500 bits of navigation data for the particular satellite (explicit time synchronisation and position computation)
- Includes corrections according to the General Theory of Relativity
- ... does not include any cryptographic protection

L1 C/A SECURITY

- Position/Velocity/Time (PVT) spoofing is accessible to a moderate-level attacker
 - real-life scenario may (allegedly) be that "Iran-U.S. RQ-170 incident"
 - actually, a GPS "replay attack" is a standard advanced tutorial for the LabView platform using the USRP Software Defined Radio (SDR)
- OK, this signal was never meant as a military-grade service and the lack of protection here can hardly be called a "discovery"
- On the other hand, a lot of commercial applications have grown up to be vital parts of our critical infrastructure today...

CIVIL GPS UNDER SERIOUS ATTACK

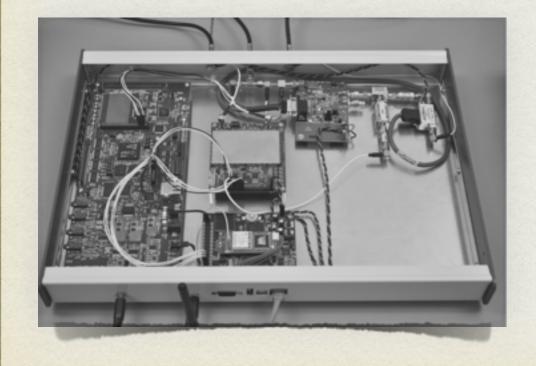


[Humphreys, Ledvina, and Shepard, 2008-2011]

PRECISE SDR SPOOFER

- receiver-spoofer architecture
- tracks original L1 C/A and L2C
- manipulates individual SV signal channels of L1 C/A (up to 12)
- re-mixes and re-transmits the spoofed signal
- precise phase sync for a smooth take over
- SDR architecture; someday it could be just downloaded and run
- HW parts were off-the-shelf components of approx. \$1500 (2008)

[Humphreys, Ledvina, and Shepard, 2008-2011]



THE NEXT TARGET?

- Recall those 37 500 bits of navigation data transmitted on each and every L1 C/A channel
- It has been observed the baseband processors in GPS user modules seldom care about the integrity of this data as well as of the plausibility of PVT results obtained
 - [Sheppard and Humphreys, 2011], [Nighswander et al., 2012]
- Interestingly, this suggests a new infection vector allowing malware installation right into the GPS receiver...
 - shall be covered in the future Cyber Threat Intelligence process

IEMI INTENTIONAL ELECTROMAGNETIC INTERFERENCE

SMARTPHONE IEMI



audio output is omitted for the clarity, as we are interested in the input path, now

SMARTPHONE IEMI



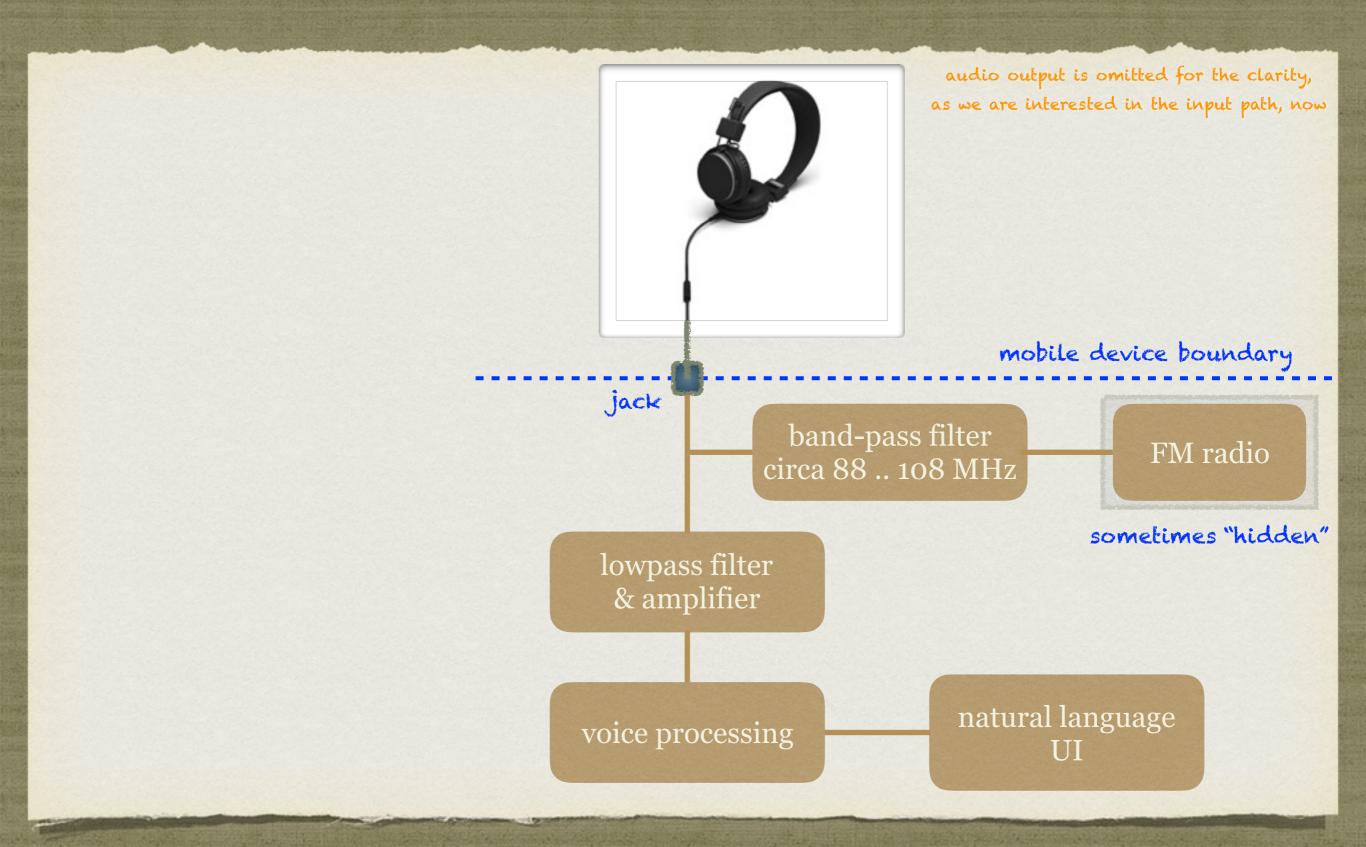
audio output is omitted for the clarity, as we are interested in the input path, now

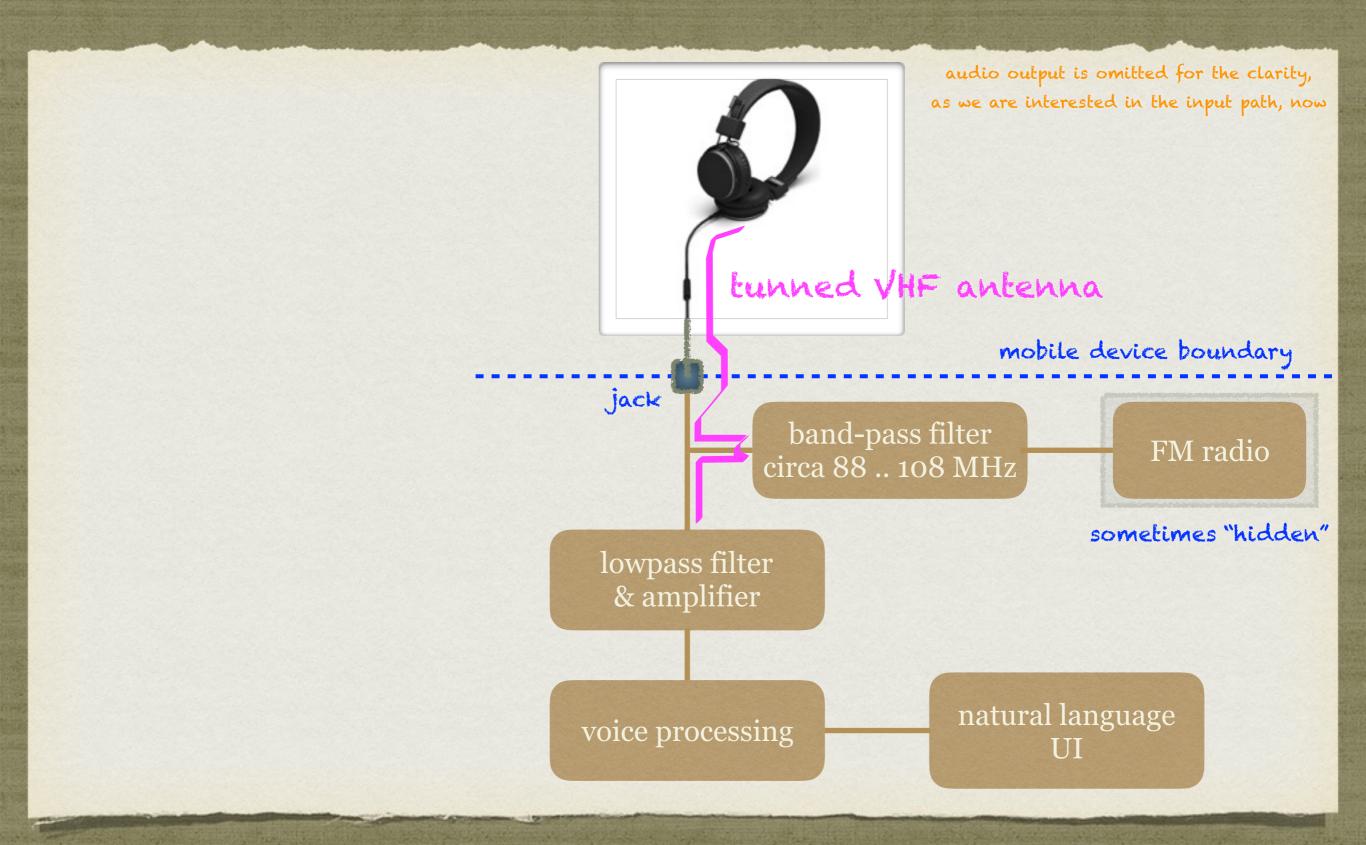
mobile device boundary

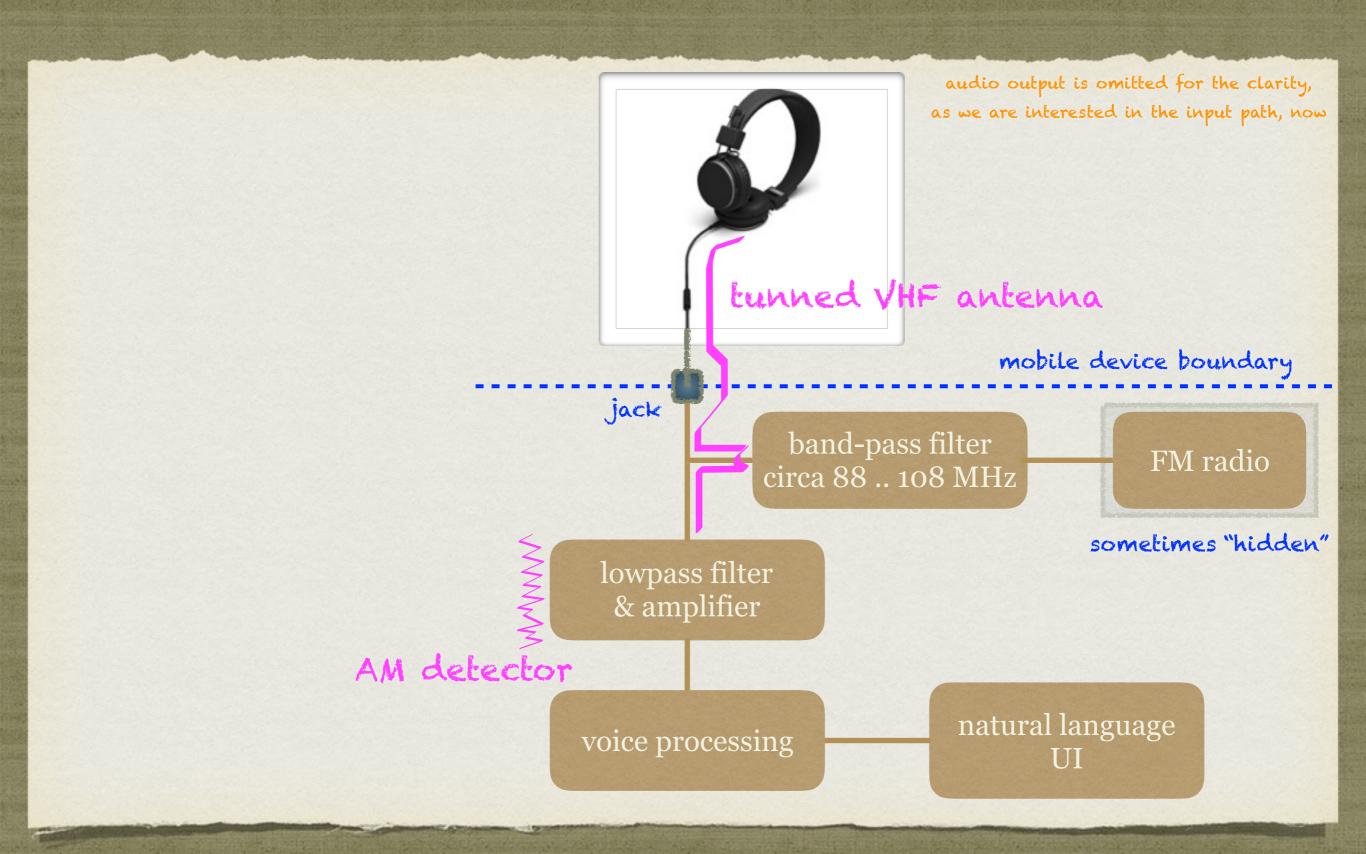


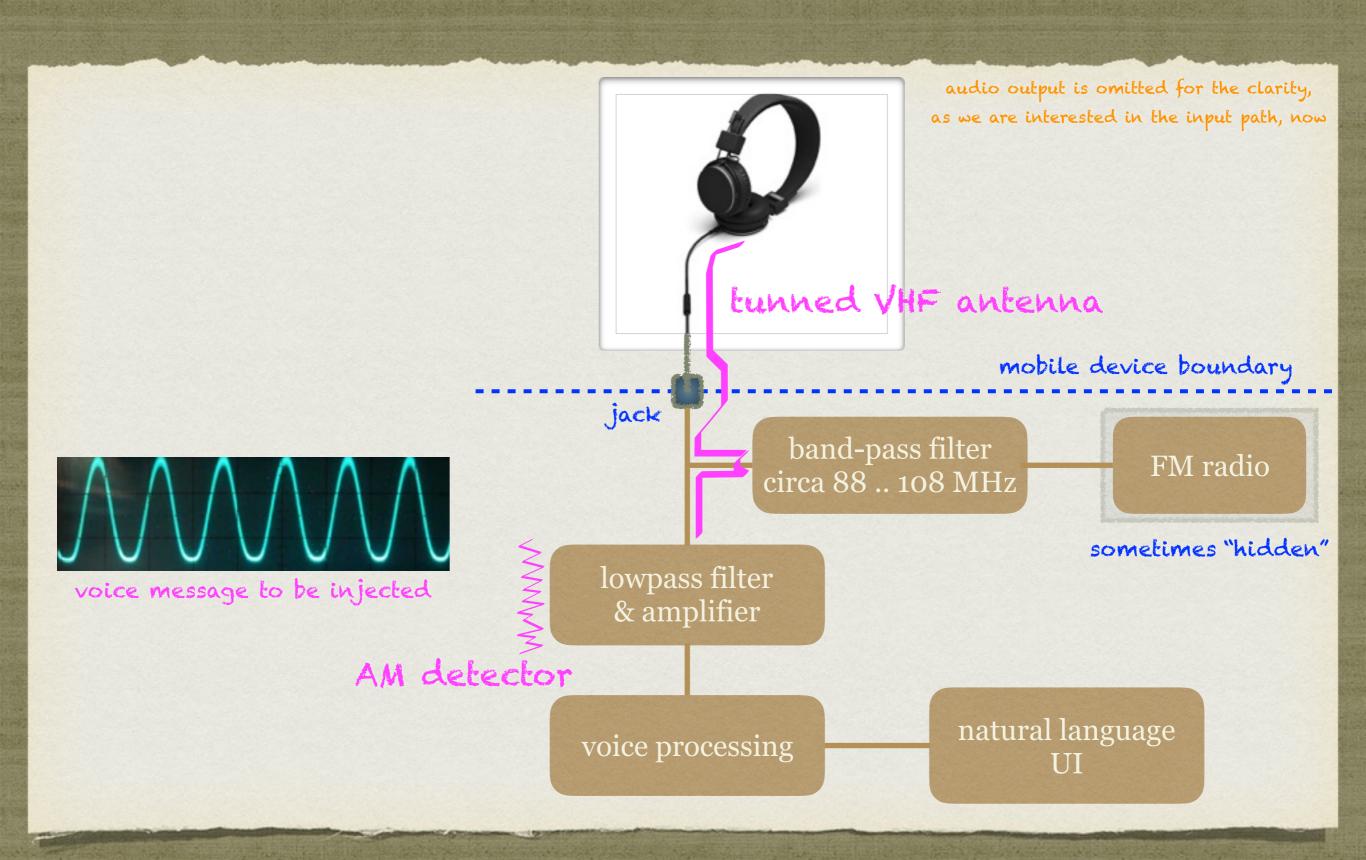


sometimes "hidden"













voice message to be injected

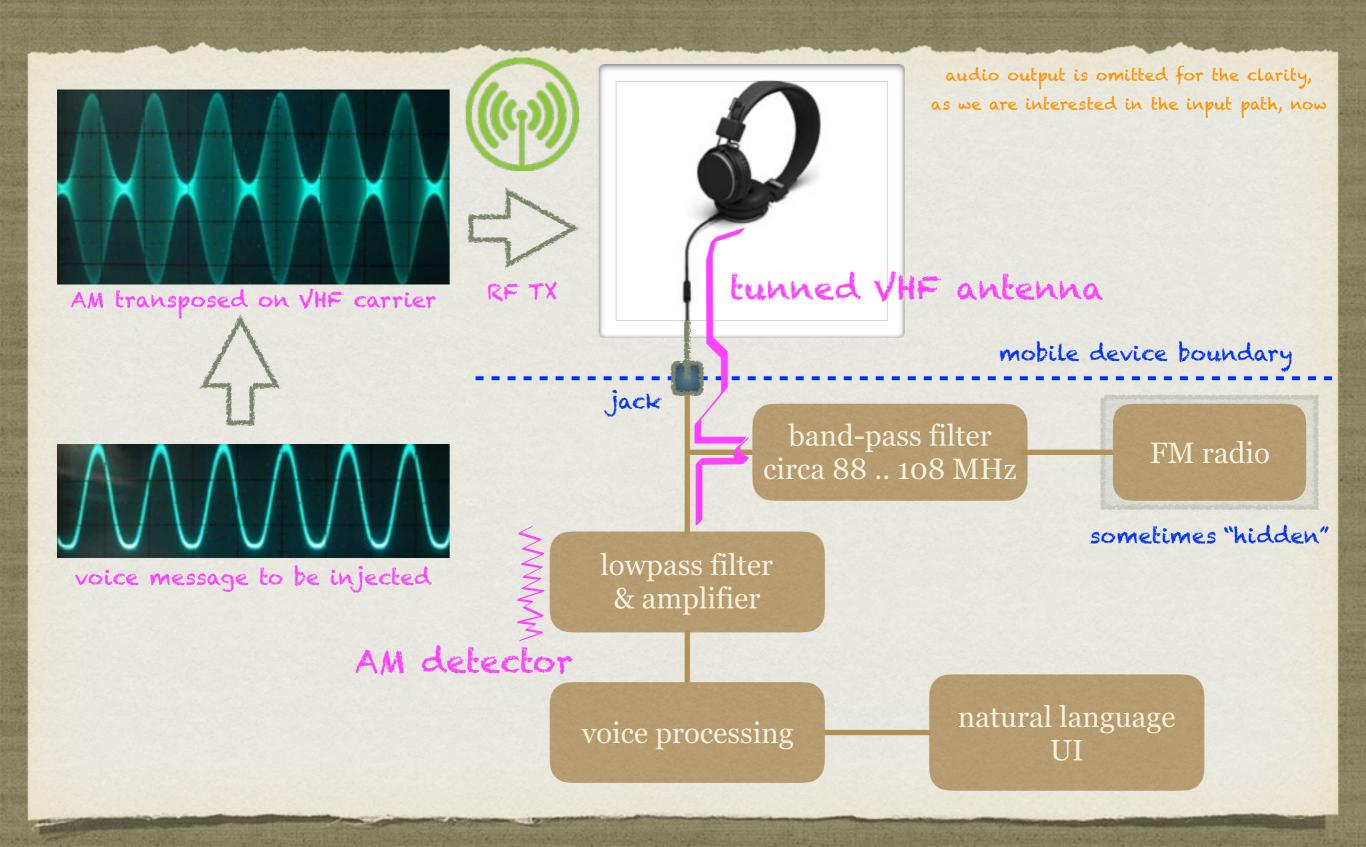


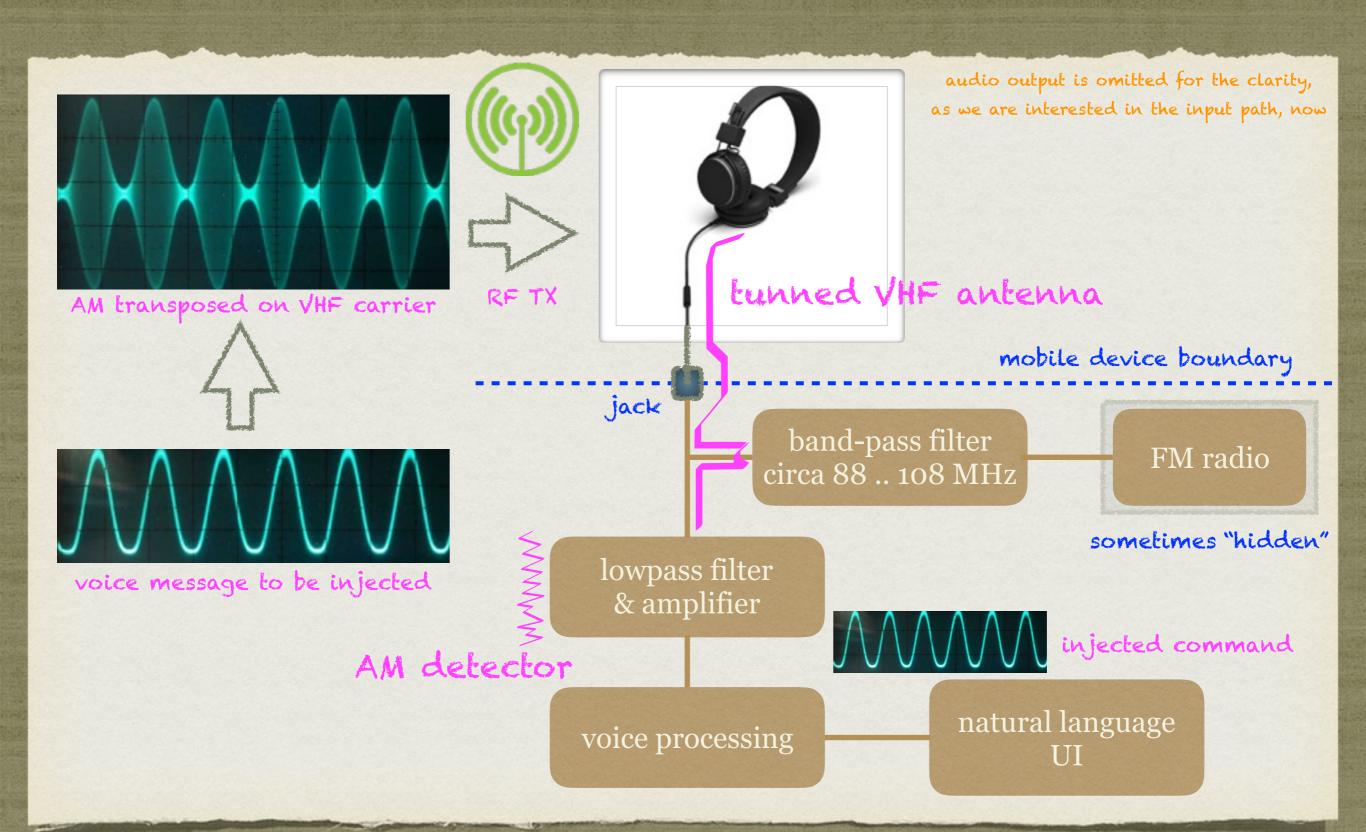
lowpass filter & amplifier

AM detector

voice processing

natural language UI





PROOF-OF-CONCEPT

- Described in [Kasmi and Esteves, 2015]
- They were able to inject voice commands into modern smartphones from the far field (Fraunhofer) region in the VHF band
 - the range was, however, still limited to several metres with a reasonable equipment
- Required $E_{\rm min} \approx 25$ 30 V/m at the victim for the 103 MHz carrier
- Interestingly, in case of the voice assistant did not listen on background, they were even able to "push" the voice command button remotely!
 - this time, it was via FM modulation of the carrier
- They employed the SDR platform with an external power amplifier

THEORETICAL IMPROVEMENTS

- Investigate higher resonant frequencies of the headphones antenna, as they can enhance the energy transfer by an intensive beam forming
- Further exploit the nonlinear distortions of the smartphone input to devise more efficient modulation schemes

CONCLUSION

- RF signals are ubiquitous, we probably cannot live without all that electromagnetic tweeting anymore
- Sometimes, our devices listen even more than they shall
- Often, the relative inaccessibility of the RF interface is the only protection
- SDR phenomenon offers easy access to the whole RF spectrum, while also allowing rapid and massive exploit sharing
- The era of intensive RF hacking is coming and it will go far beyond the usual scope of Wi-Fi and Bluetooth!
- These new attack vectors shall be included into future threat models for RF applications
- We shall require qualified penetration tests and security assessments for each and every critical RF service we have



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THANK YOU